



The low pass filter extracts the DC value and applies it to the voltage controlled oscillator, which changes the output frequency  $f_{out}$ . Since frequency synthesizer is required to produce a programmable output frequency, a frequency divider of programmable division ratio  $N$  is employed in the feedback path to divide the VCO output frequency to the one comparable to the input reference frequency. When the loop reaches steady state, the phase difference between the reference input  $f_{ref}$  and feedback signal  $f_{div}$  is constant over time and the relation  $f_{out} = N f_{ref}$  holds true. By changing the value of  $N$ , the VCO output frequency can be changed.

**III. VOLTAGE CONTROLLED OSCILLATOR**

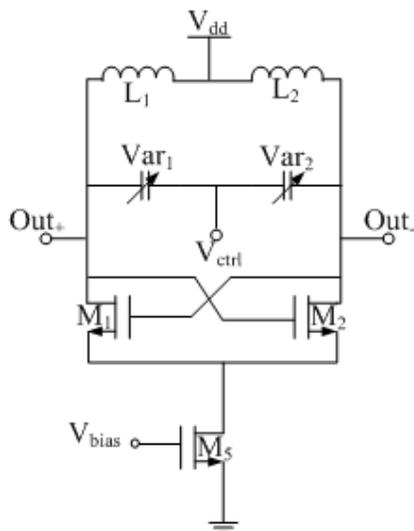


Fig. 3: Schematic of an LC VCO [3]

Fig 3 shows the conventional LC based VCO circuit design. Inductors ( $L_1$  and  $L_2$ ) and variable capacitors ( $V_{ar1}$  and  $V_{ar2}$ ) form LC tank circuit whereas cross coupled pair ( $M_1$  and  $M_2$ ) forms negative resistance.

There are various LC based VCO configurations. Mainly it includes NMOS-only, PMOS-only and complementary cross-coupled structures. For the low supply voltage NMOS only and PMOS only are used whereas complementary cross coupled structure improves the phase noise performance [4].

The oscillation frequency of LC topology is given as,

$$\omega = \frac{1}{\sqrt{LC}} \tag{1}$$

Oscillating frequency of the LC based VCO depends upon the inductance and capacitance inversely, thus frequency of oscillation is increased by decrease in inductance and capacitance value [5].

The variation in  $L$  and  $C$  are responsible for fine and course tuning of LC VCO. Theoretically, the VCO tuning range is determined by the maximum- to-minimum capacitance ratio of the varactor. For a typical capacitance ratio in a standard CMOS process, the tuning range of a LC-tank VCO is approximately limited within 30 %, making it unattractive for wideband applications [6]. To boom the VCO operating frequency range, alternative tuning mechanism is required. As an alternative tuning mechanism tunable active inductor is discussed in this paper.

**III. REALISATION OF ACTIVE INDUCTOR**

There are two fundamental approaches to realizing an active inductor using only capacitors and active gain elements. One is an operational-amplifier (op- amp) method, which can be used to design active inductors operating at moderate frequencies (up to about 100 MHz), because of the limited band-width and excessive phase shift of the op-amps.

The other approach that employs a gyrator which is the method used by almost all active inductors operating at gigahertz frequencies [7].

**Gyrator**

A gyrator consists of two back to back connected trans conductors (voltage to current converters). When one port of gyrator is connected to a capacitor, the network is called as gyrator-C network[8]. Fig 4 and 5 show the single ended active inductor connected to ground and supply voltage respectively.

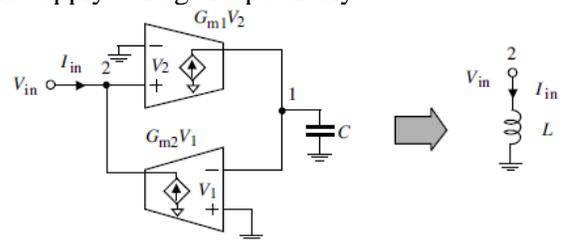


Fig.4 Lossless single ended gyrator-C active inductor connected to ground [9]

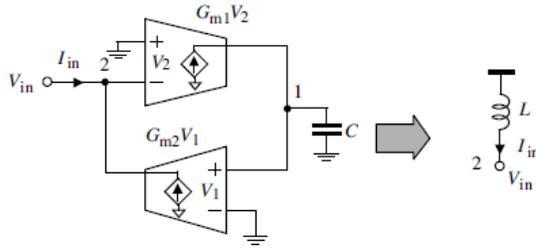


Fig.5 Lossless single ended gyrator-C active inductor connected to supply voltage [9]

To analyse gyrator-C as equivalent inductor, KCL at input port is applied. The simplified form can be explained as,

$$Z_{in} = \frac{sC}{G_{m1}G_{m2}} \quad (2)$$

The coefficient of laplace operator s shows inductance,

$$L = \frac{C}{G_{m1}G_{m2}} \quad (3)$$

In above equation input impedance  $Z_{in}$  is directly proportional to frequency, hence the impedance seen at the port 2 is inductive. This is an important property of the gyrator, which enable to synthesize an inductor.

The transistor based active inductor is developed using two trans conductors  $G_{m1}$  (positive) and  $-G_{m2}$ (negative) connected back to back in a negative feedback configuration. The topology is capable of transforming the intrinsic (parasitic) capacitance of a trans conductor to an inductance.

Although the trans conductors of Gyrator-C networks can be configured in various ways, the constraints are that the synthesized inductors should have a large frequency range, low power consumption, small silicon area and the trans conductors are to be configured as simple as possible.

Single ended and differential configured active inductors can be designed by choosing the transconductance amplifier. Common source transconductator is used for single ended negative transconductance whereas common gate and common drain are used for single ended positive trans conductance amplifier. To use floating inductor in LC VCO, differential configuration is widely used.

For spiral inductors, the quality factor of these inductors is independent of the voltage /current of the inductors. This property, however, does not hold for active inductors as the inductance of these inductors depends upon the transconductances of the trans conductors constituting the active inductors and the load capacitance. The variation of the quality factor due to the tuning of L must therefore be compensated for such that L and Q are tuned in a truly independent fashion.

Employment of CMOS active inductor in LCVCO results in number of advantages such as small die area and wide tuning range. Apart from that it also shows some disadvantages like noise due to active components, nonlinearity. VCO important parameters are as tuning range, quality factor, phase noise, output power, frequency pushing, frequency pulling, and linearity. To enhance these parameters number of trans conductance amplifier topologies can be used [10-13].

**IV.CONCLUSION**

Inception of CMOS active inductor in LC VCO results in number of advantages as compactness, tunability and wide tuning range. It also can be used to design various RF applications as low noise amplifier, power amplifier/combiner, RF filters etc. The selection of appropriate trans conductance amplifier in gyrator topology can meet the stringent parameters for RF application.

**REFERENCES**

- 1.Moon, Sung Tae, Ari Yakov Valero-Lpez, and Edgar Snchez-Sinencio. "Fully integrated frequency synthesizers: A tutorial." International journal of high speed electronics and systems 15.02 (2005): 353-375.
- 2.Manthena, Vamshi Krishna. Ultra Low Power CMOS Phase-Locked Loop Frequency Synthesizers. Diss. Nanyang Technological University, 2011.
- 3.Razavi, Behzad, and Razavi Behzad. RF microelectronics. Vol. 2. New Jersey: Prentice Hall, 1998.

4. Manthena, Vamshi Krishna. Ultra Low Power CMOS Phase-Locked Loop Frequency Synthesizers. Diss. Nanyang Technological University, 2011.
5. Srivastava, Rashmi, and Sangeeta Mangesh. "Active Inductor based VCO for High Tuning Range." *International Journal of Applied Information Systems (IJ AIS)* ISSN : 2249-0868 Foundation of Computer Science FCS, New York, USA Volume 4 No.3, September 2012.
6. Lu, L-H., H-H. Hsieh, and Y-T. Liao. "A wide tuning-range CMOS VCO with a differential tunable active inductor." *IEEE Transactions on Microwave Theory and Techniques* 54.9 (2006): 3462-3468.
7. Xiao, Haiqiao, Rolf Schaumann, and W. Robert Daasch. "High-frequency active inductor." U.S. Patent No. 7,042,317. 9 May 2006.
8. Do, Hubertus Tellegen Bernardus, Passive four terminal network for gyrating a current into a voltage. U.S. Patent No. 2,647,239. 28 Jul. 1953.
9. Yuan, Fei. CMOS active inductors and transformers: principle, implementation, and applications. Springer Science & Business Media, 2008.
10. R. Mukhopadhyay, Y. Park, P. Sen, Recon\_gurable RFICs in Si-based technologies for a compact intelligent RF frontend, *IEEE Transactions on Microwave Theory and Techniques* 53.1 (93), 2005, pp 8193.
11. , Apinunt, and A. Payne. CMOS oating active inductor and its applicationsto band-pass\_lter and oscillator designs. *IEE Proceedings-Circuits, Devices and Systems* 147.1(2000): 42-48.
12. Xiao, Haiqiao, and Rolf Schaumann, A 5.4-GHz high-Q tunable active-inductor bandpass\_lter in standard digital CMOS technology, *Analog integrated circuits and signal processing* 51.1, 2007, pp 1-9.
13. Uyanik, H. Ugur, and Nil Tarim. "Compact low voltage high-Q CMOS active inductor suitable for RF applications." *Analog integrated circuits and signal processing* 51.3 (2007): 191-194.